The objective of this program was to design and develop an automatic gain control system (subsequently referred to as AGR) for audio, which would produce a useable output level under varying ambient noise conditions. The target specifications for the unit are as follows:

- 1. Power input up to 1 mw.
- 2. Maximum power output 100 µw into a 2,000 ohm load.
- 3. Output in the absence of noise 1 to 2 microwatts with a maximum Automatic Gain Regulation of 17 to 20 db, providing an automatic control of at least 2 to 100 microwatts under noise conditions varying from 0 to maximum.
- 4. Intelligibility The Automatic Gain Regulation System will not appreciably alter intelligibility for signal levels which would normally be understandable.
- 5. Size This unit will have a volume of approximately one-half to l cubic inch and will have a flat form factor.
- 6. Power Source Operating power of the Automatic Gain Regulation Device should be derived from a small nickel cadmium storage cell which would receive charging energy by rectification of the audio input to this device.

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II. MEETINGS

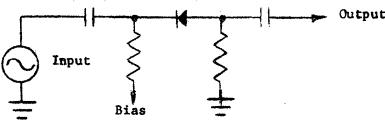
A meeting was held at ___, Philadelphia, midway through the project. At 25X1 this time, an operational breadboard was demonstrated.

III. WORK PERFORMED

a) A breadboard was built up based on an ______developed system of audio gai25X1 regulation. This system was tested and improved during the first month of the project. At the same time, other systems and methods were investigated, many of which were breadboarded and tested. None met the requirements of simplicity, attenuation range, or reliability as well as did the diode AGR system.

b) Description of the Diode Attenuator

The AGR utilizes diode conduction characteristics to obtain a variable impedance. Generally, voltage controlled attenuation circuits utilizing diode networks take advantage of the change in the resistance of diodes in the reverse bias direction. This method is unsatisfactory when used in conjunction with certain low impedance semi-conductor circuitry. The method described here is one utilizing the change in resistance of diode when it is based in the forward direction. As one examines closely the curve of forward current versus diode resistance, it is apparent that at the extreme low end of this curve there is a useable portion of variable resistance. The impedance levels associated with this device are considerably low, therefore making it compatible with other low impedance circuitry. In practice, this is a very low-level device, due to the very non-linear forward characteristic of the diode in the low bias region. The signal to be attenuated must be a very small percentage of the total diode charge. This limitation, however, allows a very large ratio of attenuation for a simple network. In practice, it has been found that voltage ratios of as much as 200 to 1 are possible, provided the correct type of diode is used. A typical circuit is shown below:



IV. THEORY OPERATION (Refer to Block Diagram - Figure 1)

The audio source delivers 1 mw maximum power to a pre-attenuator (Pre-attenuation is necessary to bring the signal into the linear forward characteristic of the diode, as described above.) The signal is then amplified in the output

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stage so that 200 µw may be delivered to the load. The signal from the microphone feeds a high-gain noise amplifier, whose output is rectified by a noise rectifier. This signal is filtered to provide the AGR voltage which then is applied to the voltage controlled attenuator.

ADDITIONAL CONSIDERATIONS

- It was originally proposed to supply 100 µw of power to the load but after further investigations and tests, it was found that in some cases under very high ambient noise conditions, more power was necessary. Therefore, the maximum power output was made to be 200 up or greater. ..
- 2. It was found that 20 db of control was adequate, as originally proposed, in order to overcome ambient noise changes.
- 3. The charge time of the system is coincidental with an incoming ambient noise signal. The discharge time constant has been selected to be generally in the area of .25 seconds. Due to the nature of the filter system, discharge time becomes longer with a larger amplitude noise input.
- 4. It was originally planned to charge the battery, from the signal, but investigation proved this to be impossible. There is not enough current developed from the signal to charge the battery. Example:

The signal power of 1 mw @ 2KΩ provides 1.4 v rms and a maximum current of 700 µa.

The battery needs minimum 2 ma to charge and at least 1.5 volts to provide the end battery voltage. Adding the unit drain of nominally 4-5 ma, this means that 6-7 ma must be available to charge the battery. As can be seen above, only 700 µa is available from the signal. Because of this, it was agreed to supply power for the unit from an external 12 volt source. Three (3) volt supply was chosen using a zener diode.

VI. FINAL SPECIFICATIONS

The specifications met by the prototype are as follows:

- 1. Power input up to 1 mw using a source impedance of 2K ohms.
- 2. Maximum power patput 200 μw into a 2000Ω load (original specification was 100 µw but this was found to be inadequate under high ambient noise conditions.

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3. Range of ga	ain regulati	on - nominal regulat	ion of 20 db (2 to 200	μw).
4. Intelligibe gibility at any signs	•	AGR system does not	appreciably alter intel	.1i-
5. The unit of power from an externa	•		cubic inch. The unit	lerives
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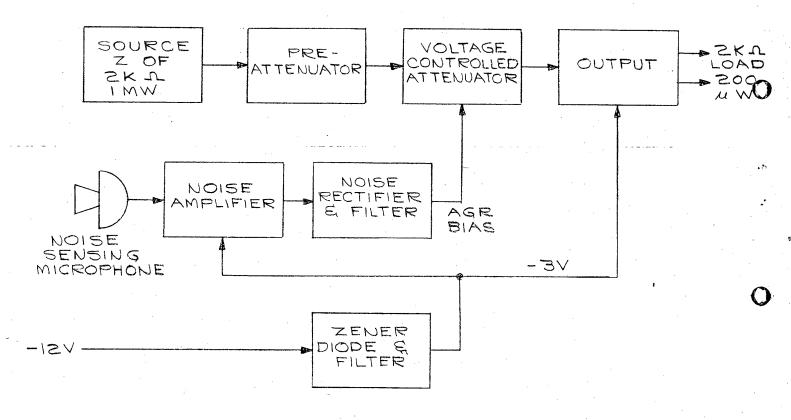
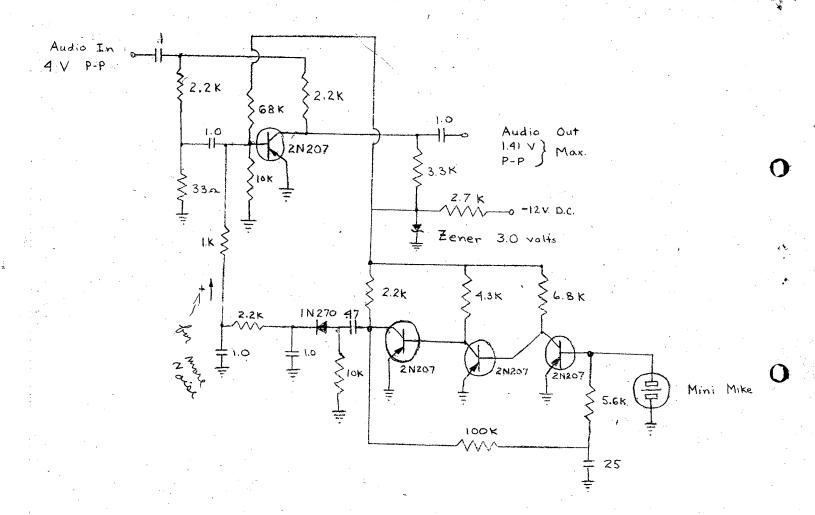
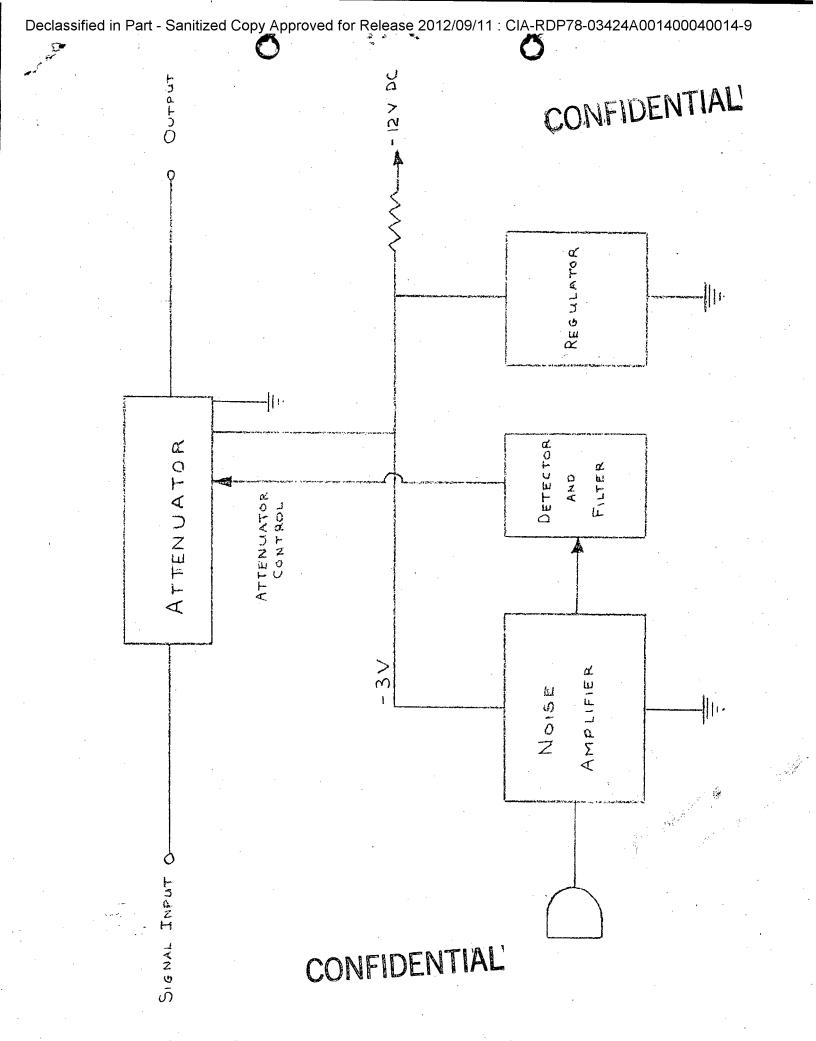


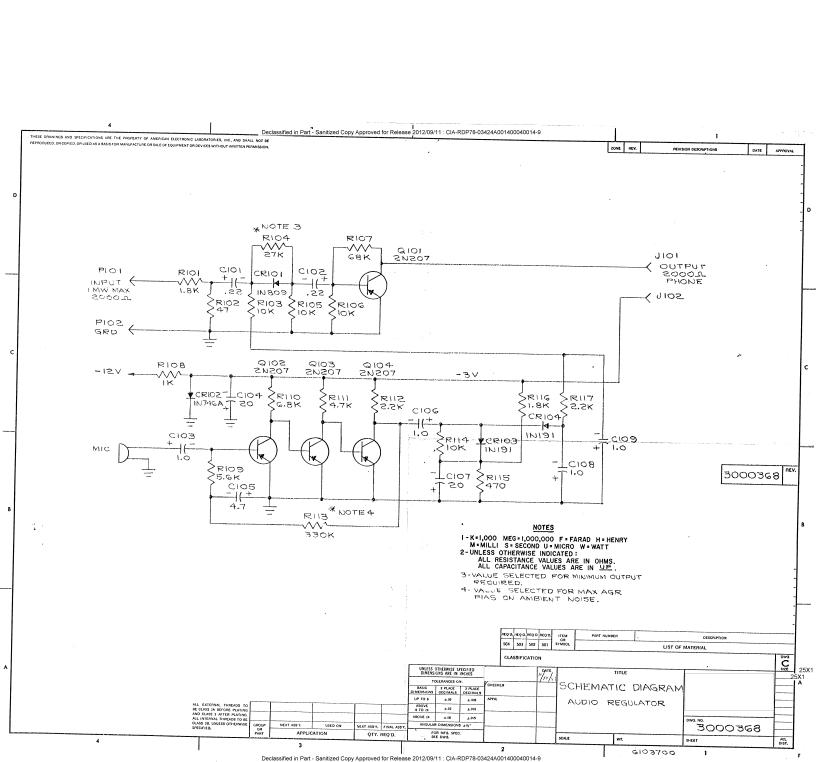
FIGURE 1 BLOCK DIAGRAM OF THE AUTOMATIC GAIN REGULATION SYSTEM

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